Evaluation of US/S₂O₈⁻² compilative process performance in the removal of Erythrosine B dye from aqueous solution

Reza Shokoohi, Abdollah Dargahi, Raheleh Amiri, Zhila Ghavami™

Department of Environmental Health Engineering, School of Public Health, Hamadan University of Medical Sciences, Hamadan, Iran

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ABSTRACT

Erythrosine B is widely used for dyeing in various applications, especially in the food industry, despite its already proved toxicity and carcinogenicity. Therefore, the purpose of this study is to evaluate the efficiency of the synthesis process of US/S₂O₈⁻² in removing erythrosine B dye from aqueous solution. In this experimental study, the removal of erythrosine B dye using combined persulfate and 40 kHz ultrasound process was studied. All reactions was conducted in a beaker of 1,000 mL in an ultrasonic bath. The effects of operational parameters such as pH of the solution (3-7), initial concentration of erythrosine B dye (10–100 mg/L), and amount of persulfate concentration (0.001–0.005 mol/L) in different contact time were investigated. The results showed that the removal efficiency increased significantly by increasing the oxidant concentration, then a steady trend was observed in the removal of erythrosine B dye. The process used US/S₂O₈-2 at pH:3, concentration of persulfate at 0.003 mol/L, and the time of 60 min for achieving the highest removal efficiency (98.91%). Ultrasonic device alone had little effect in the removal of this dye. The effects of ion changes from calcium chloride on the performance of the US/S₂O₈ process were ineffective for erythrosine B dye. The results of the US/S₂O₈⁻² process application in the removal of erythrosine B dye indicated that this process has a suitably proper ability for erythrosine B dye removal and could be used as an effective method for industrial wastewater treatment.

Keywords: US/S₂O₈⁻² process; Erythrosine B dye; Ultrasonic; Aqueous solutions

Introduction

The increasing expansion of industries and consequent discharge of wastewater into the environment have created a great deal of concern about the pollution of surface water and groundwater environmental pollution. Industrial wastewater is important because of the variety of pollutants of variable quality and quantity contained therein.^{1,2} Currently, there are about 10,000 different types of synthetic dyes, and annually more than 7×10^5 tons are produced worldwide.³ Existence of high levels of dyes with high concentrations of Chemical Oxygen Demand (COD) and low biodegradability of textile wastewater in receiving water sources, as well as increasing demand and consumption of dye

Zhila Ghavami
ghavamizh@gmail.com

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materials in industries such as textiles, rubber, plastics, pharmaceuticals, paper, leather, food and cosmetics, have led to the finding of a solution for the removal of dye materials.⁴⁻⁶ Dyes have a complex molecular structure, which is often toxic, carcinogenic (production of amine groups in anaerobic decomposition), mutagenic, non-degradable and biologically stable, which creates adverse effects when entering the environment.⁷ Erythrosine B (CI 45,430) is a well-known and significant representative of the xanthene dye class, widely used in practical applications for preparations involved in dyeing in the food industry (sweets' creams, dragees coatings, cake-decorating gels, glace and tinned cherries, sausages), cosmetic and pharmaceutical industry (pills coverage, syrups, toothpaste, lipstick, make-up products, hair-care products including sprays conditioners, shampoos, deodorants, fragrance products, soaps), despite its toxic carcinogenic effects against animals and humans.⁸⁻¹⁰ A variety of studies have been



devoted to the assessment of the acute toxicity of erythrosine B.8 The major efforts around this were initiated in the 1970s, while the US FDA instituted a partial ban on erythrosine in 1990, based on studies which indicated that high doses can cause cancer in rats, in particular thyroid tumor formation.^{8,9} Other effects are associated with bronchoconstriction, sequential vascular response, elevation of protein-bound iodide, and chromosomal damage.⁹ In spite of these concerns, the consequences of erythrosine B in the environment are less investigated, and there is inadequate documentation on its removal from aqueous effluents containing dissolved erythrosine, which is difficult to be eliminated by conventional wastewater treatments.⁸⁻¹² While almost every industrial dyeing process involves a solution of dye, water-soluble reactive and acid dyes are the most problematic pollutants as they tend to pass unaffected through conventional treatment systems. 13,14 The treatment of colored wastewater is difficult and complex due to the presence of stable and non-biodegradable aromatic compounds in the structure of dyes. 15-18 The methods used to remove dyes from these industrial wastewaters are mainly biological, chemical and physical processes. 17-19 Conventional processes such as chemical treatment, reverse osmosis and adsorption of adsorbent substrates also produce secondary pollutants of this dye, and chemical oxidation methods are not costeffective and efficient.²⁰ Physical methods often do not have the power to destroy the dyes, and the remaining sludge treatment is costly in physical methods. 19,20 Chemical methods, using strong oxidants such as ozone and chlorine, are capable of breaking up dye compounds but, due to the requirement for high doses of these use of this method materials, the uneconomical.21 In recent years, advanced oxidation processes (AOPs) have extensively considered in order to overcome the problem of dye in aquatic systems. Removal of contaminants in the advanced oxidation process is performed based on the production of free hydroxyl radicals (OH) with high oxidation potential, which convert many organic chemical compounds into minerals.²² These radicals are unstable and highly active, and are produced by chemical or photochemical reactions in situ. 23,24

Free radicals are strong oxidizing agents and quickly attack organic molecules, separating a hydrogen atom from the organic material structure. ²³⁻²⁶

Nowadays, the use of oxidizing agents, such as hydrogen peroxide, persulfate, and periodontium, has been considered by the researchers to enhance the function of oxidation processes with the aim of eliminating more organic pollutants.²⁷ The persulfate ion $(S_2O_8^{2-})$ with 2.01 oxidation-reduction potential has been used as an oxidation agent of resistant compounds in chemical removal processes.²⁸ Persulfates, as a non-selective anion, soluble and stable, have unique properties including high kinetic velocity, more stability at environmental temperatures and dependence on organic matter.²⁸ Ultraviolet waves, ultrasound waves, heat, and bivalent metals are among the most important active ingredients of persulfate, which ultimately converts persulfate into free radicals of sulfate and hydroxyl. ^{28,29} Despite the great merits of the US waves, results of numerous studies have shown that the use of US waves individually due to low efficiency and the need for long time and limited energy, is not possible on a large scale. Because of increasing efficiency of ultrasound waves and overcoming the disadvantages of them mentioned above, the use of these ultrasound waves due to their ease of use and non-production of toxic by-products, combination with other methods, has been considered. Due to the thermal decomposition of persulfate during the use of ultrasound in the activation of persulfate, several highly reactive radicals such as H •, O •2- and SO₄•- are produced.²⁶

In the study by Seidmohammadi et al. on 4-chlorophenol oxidation from chemical wastewaters using US/Fenton in an aqueous environment, the results showed that 4-chlorophenol oxidation using the combined advanced oxidation process of ultrasound and Fenton, is much better than the separate use of each method. The decomposition rate of this pollutant depends on several factors, such as pH, concentration of hydrogen peroxide as oxidizing agent, contact time, iron concentration and initial concentration of organic matter.²⁶

Considering the necessity of the removal of



dye from colored textile industrial wastewaters, and as seen through studying previous researches conducted by others, there has as yet been no study on erythrosine B dye removal from aqueous solutions using the combined process. Therefore, this study was conducted to evaluate $US/S_2O_8^{-2}$ compilative process performance on erythrosine B dye removal from aqueous solution.

Materials and Methods

This experimental study was performed on a laboratory scale in a steel reactor with dimensions of 25×13×15 cm and a volume of 2.5 L, equipped with a turbulent reservoir, a transformer, and an ultrasonic wave generator with the LUC-405 model. The samples were synthetic effluents made in the laboratory with different concentrations of erythrosine B dye. Table 1 shows the specifications of the ultrasonic device used in this research. Also, the schematic design of the reactor is presented in Fig. 1. All experiments were repeated three times and the final results were reported as mean values. Hydrochloric acid (HCl) 0.1 M and sodium hydroxide (NaOH) 0.1 M were used to adjust the pH of the solutions while being controlled by a pH meter (HACH-Ha-USA). For analysis of data, the EXCEL software was used.

Table 1. Ultrasonic device specifications

Parameter	Property
Model	LUC-405
Time range	0-99 min
Temperature range	0-50 °C
Frequency	40 KHZ
Capacity dimensions	300*55*150
Main dimensions	300*285*255
Chamber material	Stainless steel
Voltage	100 to 240v-AC,50/60Hz
Manufacturer Country	South Korea

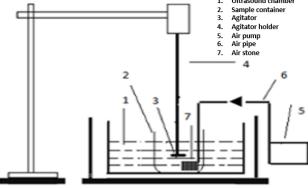


Fig. 1. Schematic design of the reactor

The acidic dye used in this study was erythrosine B dye (Ery B, CI 45,430), which was purchased from Merck Company (Germany). Its chemical structure is presented in Fig. 2. To measure the erythrosine B dye, a UV/Vis-DR 5000 spectrophotometer was used at 527 nm wavelength.³⁰

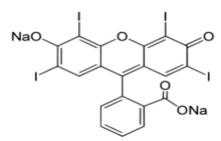


Fig. 2. Chemical structure of erythrosine B

effect of To investigate the the environmental initial pH on the process efficiency, 1,000 mL of sample with initial pH (3, 5 and 7) was entered into the reactor. Sodium hydroxide and normal sulfuric acid were used to adjust pH. Other parameters, including the initial concentration of the dye (50 mg/L), the persulfate concentration (0.003 mol/L) and the reaction time (60 min), were set. Finally, the effect of the initial pH on the specific process efficiency and on the highest efficiency was determined.

To investigate the effect of persulfate concentration on the process efficiency in removing erythrosine B dye, samples of 1,000 mL volume placed in the reactor with the optimum pH obtained in the previous step were investigated, and the concentrations of 0.001, 0.002, 0.003, 0.004 and 0.005 mol/L were analyzed. At this stage of the study, the reaction time was 60 min and the dye initial concentration was 50 mg/L. Then, at the end of the set time, sampling and measuring the residual concentration of the dve were investigated. Finally, the effect of persulfate concentration on the process efficiency was determined, and the optimal concentration was selected. Also, to determine the effect of ion intensity in the process of US/S₂O₈-2 on the removal of erythrosine B dye, CaCl₂ (0.13, 0.52 and 1.03 g/L) was added to the reactor inlet flow and the removal rate of the dye in optimum conditions of operation was measured.

In the next step, the effect of different concentrations of erythrosine B dye on the optimal conditions obtained from the previous



stages was investigated. For this purpose, the concentration ranges of erythrosine B dye, 10–100 mg/L (10, 25, 50, 75 and 100 mg/L) were considered. Also, to determine the effect of reaction time on the efficiency of the US/S₂O₈-² process, sampling was done at all stages of the studying the time range of 2.5–60 min.

Results and Discussion

Speed of chemical reactions is dependent on the pH of the environment, and the pH affects directly and indirectly the oxidation of organic matter. In advanced oxidation processes, pH changes through the production of various radicals affect the oxidation of organic matter.^{2,31} Since the pH of the solution has a direct effect on the production of hydroxyl radicals and thus can affect the efficiency of the oxidation process, the first parameter examined by the process is pH. ^{32,33} In this study, in order to verify the effect of pH in the US/S₂O₈-2 process, pH values of 3, 5, and 7 were evaluated, and the results are presented in Fig. 3. The results show that the maximum removal rate of erythrosine B was at pH:3 and contact time 60 min (98.91%), and the lowest removal rate was at pH:7 and contact time 2.5 min (10.2%). Comparison of the changes made in the first 30 min of the reaction shows that the removal efficiency at pH 3, 5, and 7 was 88.66, 81.83, and 39.41%, respectively. According to the results obtained in this study, it was found that the process efficiency in acidic pH was higher than in neutral pH. In the US/S₂O₈-2 process in acidic pH (pH:3), radical sulfate production from anion persulfate was higher in acid pH than other pHs. These findings correspond with those of the study by Apostol et al. 30 As the results of the study by Apostol et al. showed, the highest erythrosine B removal rate was found in acidic pH. Also, the results of the study by Okoye et al. showed that the highest erythrosine B removal rate was in the lowest pH value.34 As the reduction of pH from 10 to 2, the erythrosine B removal rate increased from 41% to 95.75%. Anion persulfate are one of the anions in persulfate coupled systems. Anion degradation of persulfates can lead to a decrease in the pH of the system and high pH changes in one process result in the removal of a high percentage of a pollutant.³⁵ Therefore, pH directly affects the

activation process of persulfate and can produce different radicals and anions, all of which affect the activation of persulfate and pollutant removal.^{35,36}

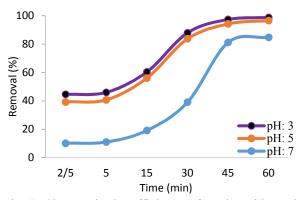


Fig. 3. Changes in the efficiency of erythrombin B dye removal at different pH and contact time in the $US/S_2O_8^{2-}$ process (concentration of erythrysine B, 50 mg/L and persulfate, 0.003 mol/L)

In order to determine the effect of changes in the concentration of persulfate on the removal of erythrosine B dye, the optimum pH was 3 and the concentration of erythrosine B was considered to be equal to 50 mg/L. The results of changes in the persulfate concentration in the US/S₂O₈²⁻ process at different contact times showed that, by adding 0.001, 0.002, 0.003, 0.004, 0.005 mol/L persulfate at 60 min, erythrosine B with an initial concentration of 50 mg/L was obtained in 69.63%, 82.08%, 98.28%, 98.48%, 99.76%, respectively (Fig. 4).

Considering that the radical hydroxyl of the combined system is greater than the differential ultrasonic system, the combined oxidation velocity will be higher than the ultrasonic separation system.³⁷ According to the results, the optimum persulfate content was chosen as 0.003 mol/L. Radical sulfate is a result of the decomposition of persulfate anions (an extremely powerful single oxidizing agent with high oxidation and reduction potential), and is likely to be competitive with radical hydroxyl and reacts rapidly with many organic materials.

In the ultrasonic/ persulfate process, the increase in the oxidizing agent concentration up to 0.003 mol/L increased the reaction speed, and with increasing concentrations of persulfate to 0.005 mol/L, the increasing trend remained constant and no change was observed. This result corresponds with results of the study by Seidmohammadi et al.²⁶, which showed that by



increasing the oxidizing matter spike to a certain extent, the reaction rate was increased, and with the increase of persulfate concentration to more than 0.02 mol/L, there was a reverse trend in removal of organic matter. Persulfates are able to produce two radicals and an hydroxyl, and these two radicals may have synergistic effects. But studies have shown that radical hydroxyl plays most of the role of the radical sulfate radicals, and does not have much effect on persulfate-derived processes.²⁶ In a study by Azadbakht et al. using a persulfate-based advanced oxidation process to metronidazole from aqueous solutions, the results showed that with increasing persulfate concentration, the efficiency of metronidazole elimination increased, 38 which corresponds with the findings of the present study. In the study of Wu et al. regarding removal of acid orange 7 by activated persulfate with electric methods, the results showed that with increased persulfate concentration from 2 to 12 mmol/ L, efficiency increased.³⁹

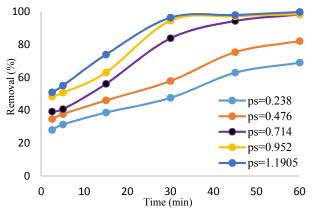


Fig. 4. Changes in the removal efficiency of erythrombin B dye in different concentrations of persulfate in the $US/S_2O_8^{2-}$ process (pH:3; concentration of erythrosine B dye, 50 mg/L)

In the next step, the effect of different concentrations of erythrosine B (10, 25, 50, 75 and 100 mg/L) on the efficiency of the US/S₂O₈² process was investigated. According to the results, by increasing the initial concentration of erythrosine B, the removal decreased. efficiency As the concentration of erythrosine B increased from 25 to 100 mg/L, the removal rate decreased from 99.29% to 69.65% after 60 min (Fig. 5). This was in agreement with the results of the study by Jain et al. 40, which showed that by reducing the erythrosine B dye concentration, the adsorbent efficiency in the removal of erythrosine B dye was increased.

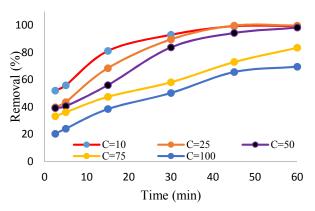


Fig. 5. Changes in the efficiency of removal of erythrosine B dye in different dye concentrations in the US/S₂O₈²-process (pH:3; concentration of persulfate, 0.003 mol/L)

In order to effect the separation of processes in the removal of erythrosine B dye under optimal conditions, which is the US/S₂O₈²- process, persulfate was studied under optimal conditions of operation and US waves alone. As the results showed, the highest removal rate of erythrosine B dye by US/S₂O₈²process (98.28%) and the lowest removal rate by the US process (28.61%) were obtained (Fig. 6). Also, the effect of persulfate alone on the removal of erythrosine B dye under optimal conditions of 63% of erythrosine B was destructured. In the case of using the US/S₂O₈²process, for 60 min, the removal efficiency increased to 99%. Thus, it can be concluded that using the US/S₂O₈²- process was 1.5 times faster than persulfate and 4.5 times faster than ultrasonic waves in eliminating erythrosine B dve.

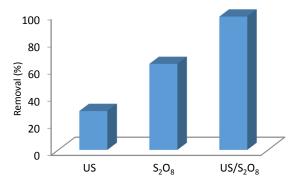


Fig. 6. Comparative removal efficiency of erythrosine B dye in the US/S₂O₈²-process, with persulfate in optimal conditions of operation, and US waves alone (pH:3; initial concentration of dye, 50 mg/L, and concentration of persulfate, 0.003 mol/L)



In order to influence the changes in calcium chloride concentration in the US/S₂O₈² process, to remove the erythrosine B dye, the concentration of calcium chloride in the range of 0.13 to 1.3 mg/L was investigated. The results showed that increased concentration of calcium chloride did not have a significant effect on dye removal. In the concentration of calcium chloride equal to 0.13, 0.52 and 1.03 g/L, the removal rate of erythrosine B dye was 96.71%, 97.5% and 97.81%, respectively, for 60 min (Fig. 7). Therefore, according to Fig. 6, it can be concluded that the variations in ionic intensity have been slightly reduced in the US/S₂O₈²process. Probably this phenomenon can be due to the activation of persulfates and other active radical species that were formed in high concentrations of persulfate and caused ion interference. This finding is similar to those of the study by Seidmohammadi et al., where, with increasing calcium chloride ion intensity, the efficiency of metronidazole removal increased.41

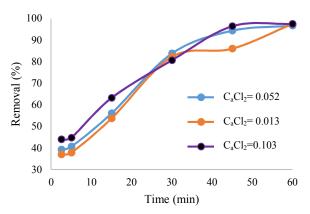


Fig. 7. Changes in the efficiency of removal of erythrosine B dye in different concentrations of sodium chloride in the $US/S_2O_8^{2-}$ process (pH: 3; initial concentration of dye, 50 mg/L and concentration of persulfate, 0.003 mol/L)

Conclusion

The US/S₂O₈²⁻ process is a very effective process for the destruction of erythrosine B dye from aqueous solutions. The performance of the US/S₂O₈²⁻ process in optimal conditions for erythrosine B dye indicates high removal efficiency, so that at least 60 min of the US/S₂O₈²⁻ process eliminated more than 90% of the erythrosine B dye. This process can also be used as an effective method to remove this dye from industrial wastewater.

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